

DOI: <https://doi.org/10.23670/IRJ.2023.130.6>**METHOD OF HARMONIC ANALYSIS OF CIRCUMFERENTIAL IRREGULARITY OF STEAM FLOW DOWNSTREAM THE TURBINE ROTARY DIAPHRAGM**

Research article

Ilichev V.Y.^{1,*}, Zhinov A.A.², Shevelev D.V.³¹ ORCID : 0000-0003-1017-5544;² ORCID : 0000-0002-6409-4777;³ ORCID : 0000-0002-7104-3249;^{1,2,3} Bauman Moscow State Technical University, Kaluga, Russian Federation

* Corresponding author (patrol8[at]yandex.ru)

Abstract

Control stage with rotary diaphragm at heat extraction of steam turbine is considered. A method for building a 3D model of the control diaphragm of the turbine stage has been developed for its further study. Methods of numerical experiment investigated the unevenness of the velocity field behind the nozzle guide vanes of the considered turbine stage. The developed technique has been tested in various operating modes of the rotary diaphragm. It was found that for the considered stage, the dynamic component of the circumferential unevenness of the flow upstream of the rotor blades significantly exceeded the dynamic component of the unevenness of the flow along the height of the blades. A significant range of speed pulsations was noted, reaching 200... 250 m/s with a maximum steam speed of 455 m/s. Spectral analysis of the obtained velocity field was carried out, which made it possible to determine potentially dangerous frequencies of pulsation of steam force. Steam flow pulsation frequencies are compared with natural frequencies of turbine impeller blades, resonance conditions are found. This makes it possible to find and determine the possible dangerous frequencies of the variable aerodynamic force acting on the rotor blades of the stage with the rotary diaphragm, from the combination of the spectrum of frequencies of harmonics of the circumferential unevenness of the flow and the spectrum of natural frequencies of vibrations of the blades (a set of blades, the entire rim of the blades) in different modes of operation of the turbine.

Keywords: steam turbine, CFD, rotary orifice, simulation, resonance.**МЕТОДИКА ГАРМОНИЧЕСКОГО АНАЛИЗА ОКРУЖНОЙ НЕРАВНОМЕРНОСТИ ПОТОКА ПАРА ЗА ПОВОРОТНОЙ ДИАФРАГМОЙ ТУРБИНЫ**

Научная статья

Ильичев В.Ю.^{1,*}, Жинов А.А.², Шевелев Д.В.³¹ ORCID : 0000-0003-1017-5544;² ORCID : 0000-0002-6409-4777;³ ORCID : 0000-0002-7104-3249;^{1,2,3} Московский государственный технический университет имени Н.Э. Баумана, Калуга, Российская Федерация

* Корреспондирующий автор (patrol8[at]yandex.ru)

Аннотация

Рассмотрена регулирующая ступень с поворотной диафрагмой на теплофикационном отборе паровой турбины. Разработана методика построения 3D-модели регулирующей диафрагмы ступени турбины для её дальнейшего исследования. Методами численного эксперимента исследована неравномерность поля скоростей за сопловым аппаратом рассмотренной ступени турбины. Разработанная методика апробирована на различных режимах работы поворотной диафрагмы. Установлено, что для рассмотренной ступени динамическая составляющая окружной неравномерности потока перед рабочими лопатками значительно превышала динамическую составляющую неравномерности потока по высоте лопаток. Отмечен значительный размах пульсаций скорости, достигающий 200... 250 м/с при максимальной скорости пара 455 м/с. Проведен спектральный анализ полученного поля скоростей, позволивший определить потенциально опасные частоты пульсации парового усилия. Выполнено сопоставление частот пульсации парового потока с собственными частотами лопаток рабочего колеса турбины, найдены условия возникновения резонанса. Это делает возможным поиск и определение возможных опасных частот переменной аэродинамической силы, действующих на рабочие лопатки ступени с поворотной диафрагмой, от совмещения спектра частот гармоник окружной неравномерности потока и спектра собственных частот колебаний лопаток (пакета лопаток, всего венца лопаток) на различных режимах работы турбины.

Ключевые слова: паровая турбина, CFD, поворотная диафрагма, моделирование, резонанс.**Introduction**

The reliability of the steam turbine plant is largely determined by the accident-free operation of the turbine, which, first of all, depends on the reliability of the operation of its blade apparatus, as well as its regulators – valves and rotary diaphragms [1], [3], [4], [5]. Rotor blades of steam turbines are one of the most loaded elements of the turbomachine design. Numerous cases of emergency destruction of blades are known, which led to complete failure of the entire turbine plant [1], [4]. The reasons leading to the destruction of the blades are diverse: from errors in their design and manufacture, to the impossibility of complete quality control of structural materials, as well as erosion wear and operation in non-design modes. One of the most

important parameters that determine the dynamic strength of the blades and the fatigue stresses in them are the values and frequencies of disturbing forces acting on the side of the incoming flow onto the blades. The frequencies of these forces are always a multiple of the rotor speed of the turbine, but its harmonic composition significantly depends on the design of the flow path both before and after the blades in question. The most dangerous, in terms of resonant phenomena of the blade apparatus, are frequencies up to the 6th harmonic of the natural frequency of the blades inclusive. However, modern data indicate a danger and higher frequency harmonics, up to 8-9 [6]. Thus, harmonic analysis of the dependence of the disturbance force on the circumferential unevenness of the flow acting on the blades is an extremely important task.

In the design of many steam turbines with adjustable steam extraction, control stages with rotary diaphragms are provided. Before the rotor blades of such stages, an uneven flow of steam is formed along the circumference, the characteristics of which depend both on the design of a particular diaphragm and on the mode of its operation, that is, the degree of its opening. Analytically, it is not possible to obtain characteristics of such unevenness, due to the complex spatial nature of the current. It is proposed to solve this problem by numerical modeling [7] according to the methodology presented below.

One of the main objectives of simulation of aerodynamic processes in the rotary diaphragm and nozzle grating of the control stage is harmonic analysis [8] of flow heterogeneity in the gap between the nozzle and working grating in order to obtain the frequency spectrum of harmonics of the disturbing force acting from the flow side on the rotor blades during turbine operation.

Research methods and principles

When implementing the proposed procedure, a control stage with a rotary diaphragm was considered at the heat extraction of the steam power turbine of the steam-gas plant [9]. Modeling was carried out using a three-dimensional model of the system: rotary diaphragm – intermediate chambers with partitions – nozzle grating. For the convenience of modeling and evaluating the results, this model is converted into a flat pattern by the average diameter of this turbine stage. For the flow sections of the reaming of the fixed and rotary ring of the diaphragm, the equality of the sections of the nozzle guide vanes and the meridional section of the diaphragm model was maintained.

The model created by the authors is shown in Figure 1; it allows you to obtain any degree of opening of the rotary diaphragm by moving the scan of the model of the rotary ring of the diaphragm relative to the scan of the stationary ring.

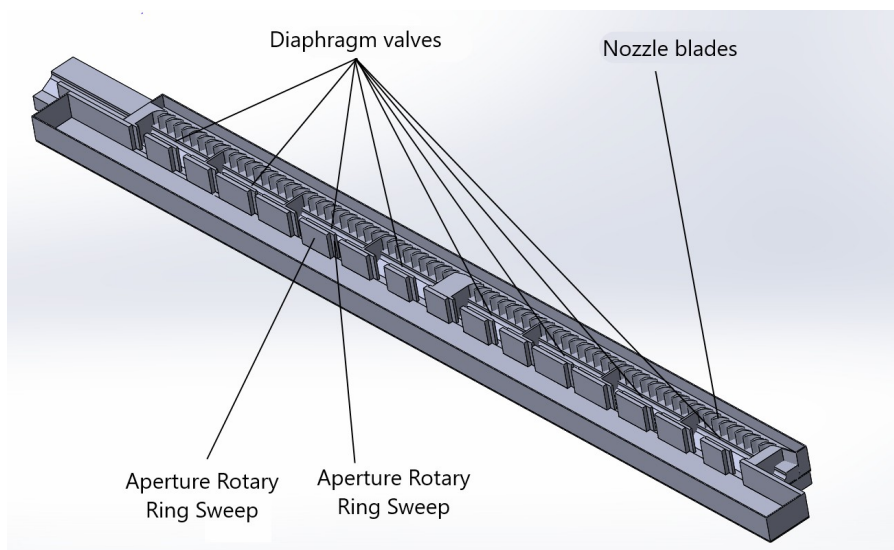


Figure 1 - System model: rotary diaphragm - intermediate chambers with partitions - nozzle grating

DOI: <https://doi.org/10.23670/IRJ.2023.130.6.1>

The boundary conditions imposed on the model corresponded to the thermodynamic parameters characteristic of the considered turbine operation mode. Modes from full closure to full aperture opening were simulated.

The mathematical model of the flow of compressible viscous gas (water vapor) was based on a system of classical equations for preserving mass, momentum and energy. The k-e model [10] was used as a turbulence model.

A calculated grid was built in the volume of the design model. To increase the accuracy of modeling, it was adapted – local grinding in critical areas of the calculated area – in the area of models of aperture windows, internal volume of cavities, inter-blade channels of the nozzle assembly.

Figure 2 shows a fragment of the calculated grid of the calculated region of the model. The total number of calculated cells in the entire simulated region is more than 8 million.

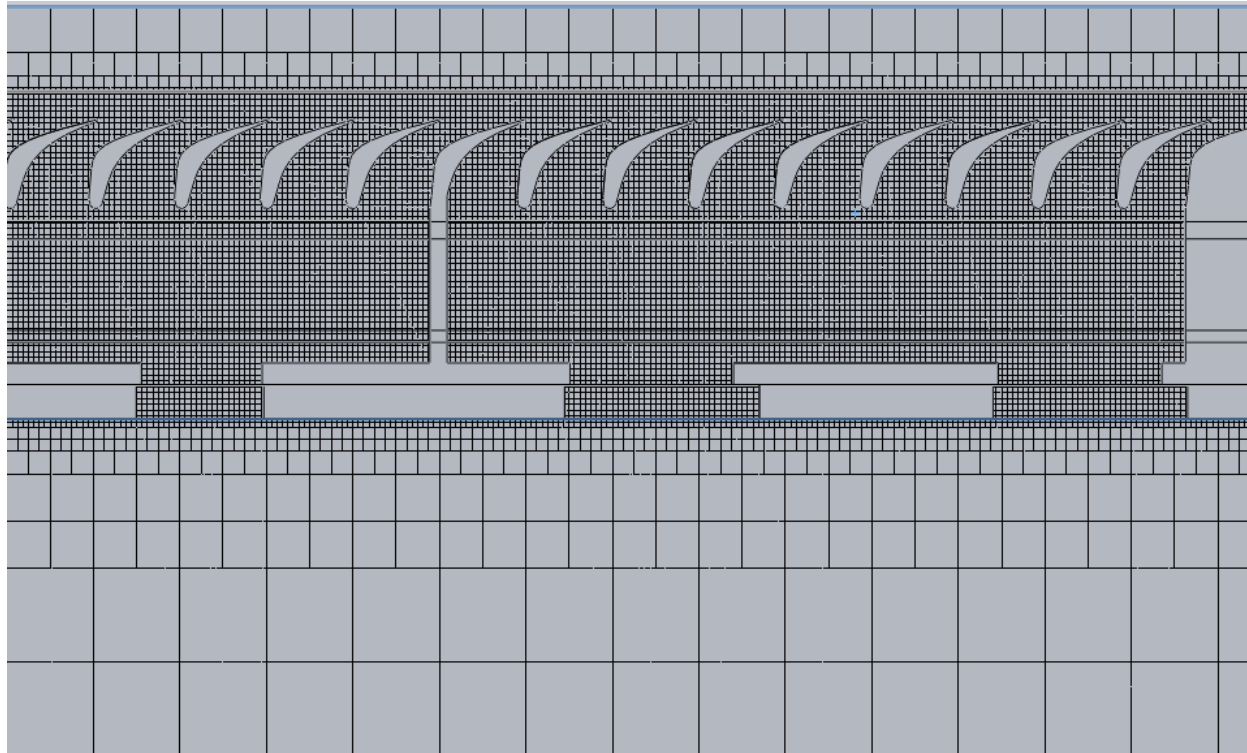


Figure 2 - Fragment of the calculated grid
DOI: <https://doi.org/10.23670/IRJ.2023.130.6.2>

Main results

The condensation mode of the turbine [11] provides for the complete opening of the windows of the rotary diaphragm. Results of steam flow simulation in condensation mode are shown in Figures 3 and 4.

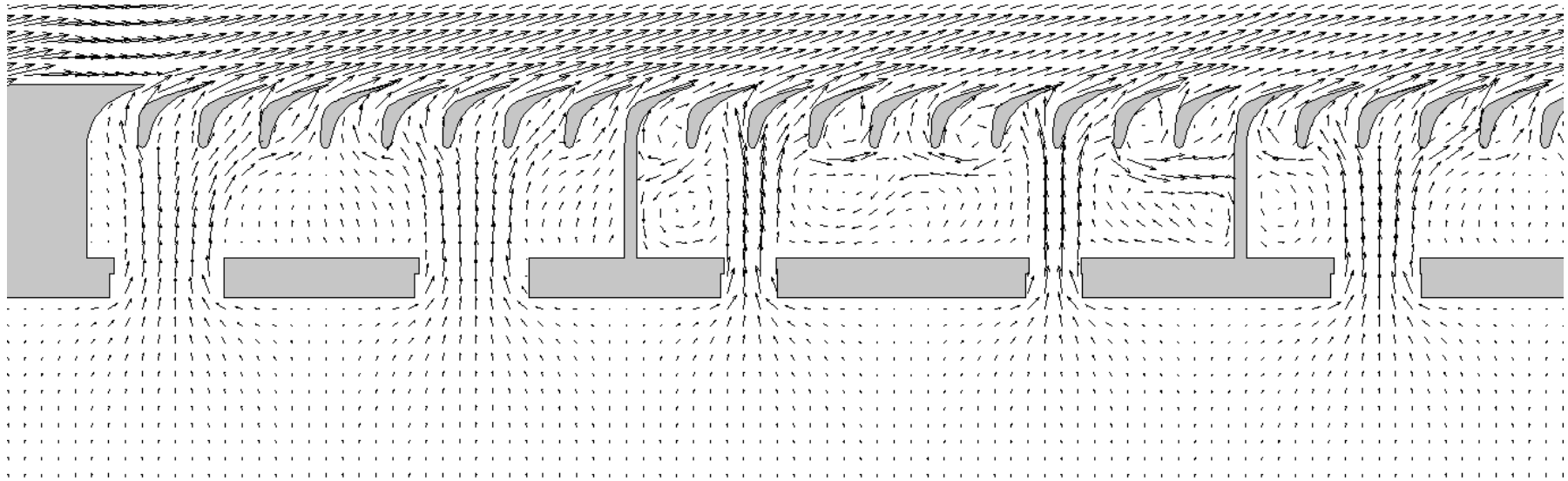


Figure 3 - Vapor velocity vectors on the characteristic portion of the diaphragm when the diaphragm is fully opened on the middle diameter
DOI: <https://doi.org/10.23670/IRJ.2023.130.6.3>

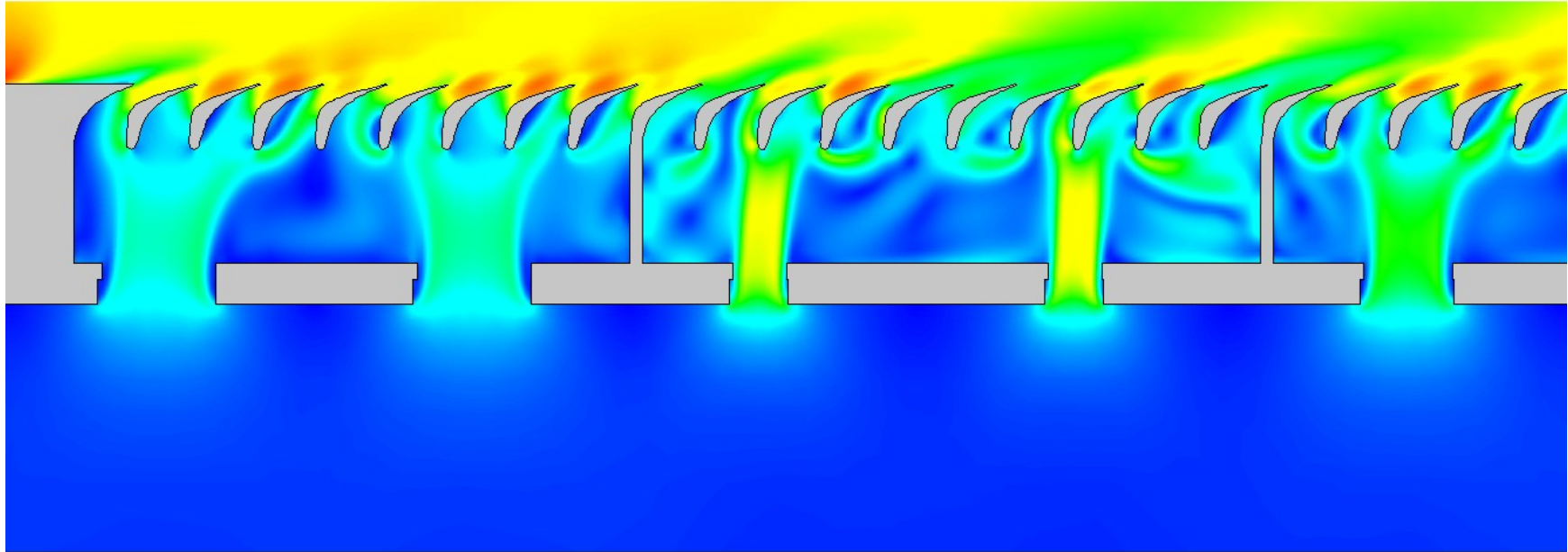


Figure 4 - The steam velocity field in the characteristic section when the diaphragm is fully opened at the middle diameter of the control stage
DOI: <https://doi.org/10.23670/IRJ.2023.130.6.4>

From the presented figures, it can be seen that behind the open openings of the diaphragm, a complex jet flow of steam is formed with the formation of spatial stagnation zones and vortex currents in the chambers between the diaphragm and the nozzle grating. Steam jets reach the nozzle grating and form considerable non-uniformity of velocity field behind it. Change of steam velocity at the inlet to the working grid, at the level of leading edges of the rotor blades in the considered mode, along the circumference length at the middle diameter of the control stage is shown in Figure 5.

It can be seen from Figures 3, 4 and 5 that the steam exiting through the windows of the rotary diaphragm forms a non-uniform flow in the diaphragm cavities. Steam flow rate in nozzle channels within each cavity is different. Most of the steam, in this mode, passes through nozzle channels located opposite the open windows of the rotary diaphragm.

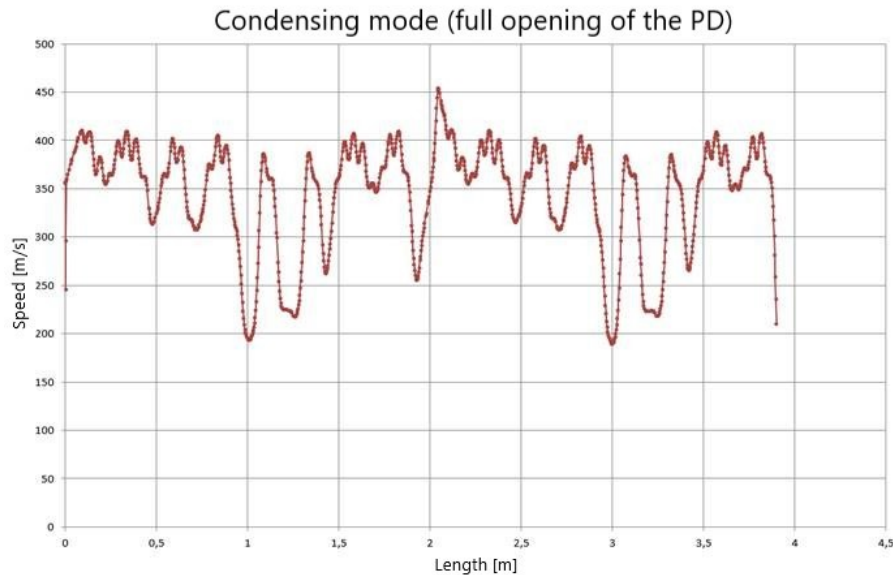


Figure 5 - Change in the steam velocity at the inlet to the working grid when the diaphragm is fully opened along the circumference on the middle diameter of the stage
DOI: <https://doi.org/10.23670/IRJ.2023.130.6.5>

Modeling showed that for the stage under consideration, the dynamic component of the circumferential unevenness of the flow upstream of the blades significantly exceeded the dynamic component of the unevenness of the flow along the height of the blades, therefore, to obtain a spectral analysis of the disturbance force acting on the blades, only the circumferential component of the unevenness of the flow on the middle diameter of the stage was used.

Steam speed pulsations in front of the rotor blades, in the considered mode, at each rotation of the rotor have a significant span reaching 200... 250 m/s with a maximum steam speed of 455 m/s. These velocity pulsations form significant steam force pulsations on the rotor blades.

In order to determine the potentially hazardous frequencies of steam force pulsation, the spectral analysis of the dependence presented in Figure 5 was carried out. The results of spectral analysis of the circumferential irregularity of the steam flow upstream of the blades in condensation mode are shown in Figure 6. It is obtained that harmonics with the highest amplitudes are multiples of 100 Hz, while the maximum amplitude has harmonics of 800 Hz and 100 Hz.

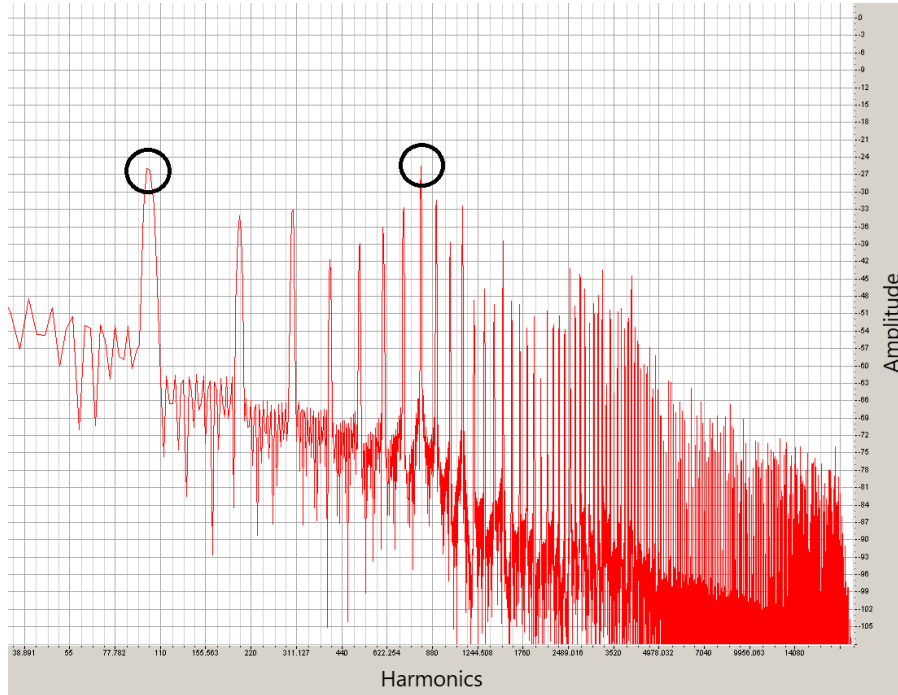


Figure 6 - Results of spectral analysis of circumferential irregularity of steam flow upstream of rotor blades in condensation mode:

circles - largest amplitude

DOI: <https://doi.org/10.23670/IRJ.2023.130.6.6>

Harmonic with maximum amplitude – 800 Hz is determined by the number of windows opened in this mode – 16 (16 * 50 Hz = 800 Hz). Harmonics 100 Hz – the presence of two sections on the diaphragm without nozzle blades near the horizontal connector of the turbine housing. The harmonic 4100 Hz is also detected – formed by edge traces of nozzle blades, but its amplitude is relatively small.

During testing of the proposed method, other operating modes of the rotary diaphragm under different operating modes of the diaphragm were investigated. For example, Figure 7 shows the results of spectral analysis of the circumferential unevenness of the steam flow upstream of the blades in a partially closed diaphragm heating mode. For this mode, the harmonic with a frequency of 100 Hz gives the largest amplitude of the disturbance force.

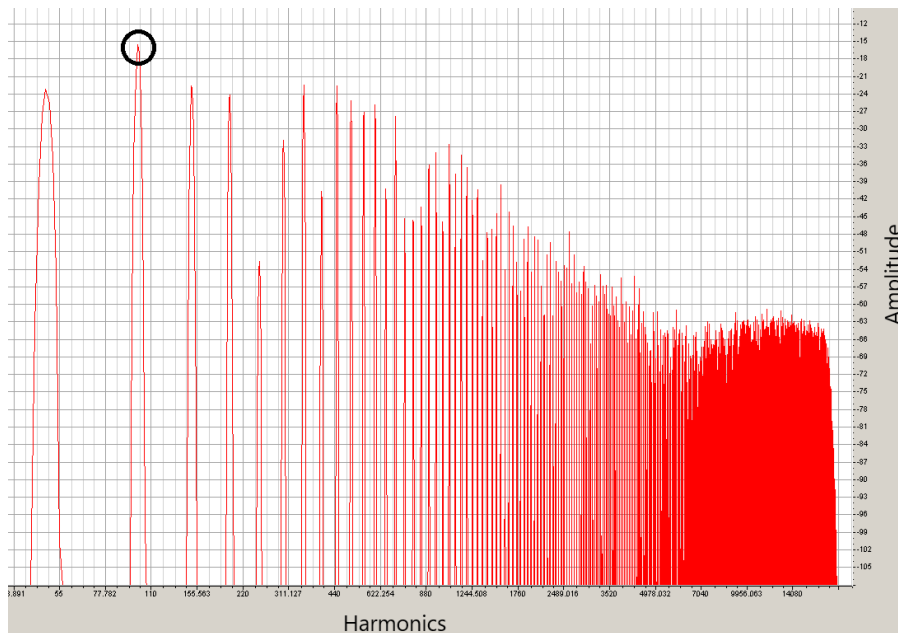


Figure 7 - Results of spectral analysis of circumferential irregularity of steam flow upstream of rotor blades at heating mode:

circle - largest amplitude

DOI: <https://doi.org/10.23670/IRJ.2023.130.6.7>

Discussion

The variable field of flow rates in the circumferential direction at the outlet of the nozzle assembly is the cause of pulsation of the aerodynamic force (steam force) acting on the rotor blades of the turbine stage in question. This, in turn, leads to the emergence of alternating stresses that affect the strength characteristics of the rotor blades.

The coincidence of harmonic frequencies with the maximum amplitude of this force with the natural frequencies of the blade rim is especially dangerous, while resonant phenomena and destruction of the blades are possible [12].

Natural frequencies and forms of vibrations of rotor blades (blade stack, the whole blade rim of the considered stage) were also determined by numerical methods in specialized software. Harmonics up to and including 9 were considered potentially dangerous.

It is almost impossible to accurately determine the magnitude and direction of the variable aerodynamic force acting on each rotor blade. This requires the calculation of the unsteady process of steam flow in the flow part and detailed modeling of tear currents, both in the diaphragm and within the nozzle and working grids, but it is known that the harmonics of non-uniformity of steam flow and aerodynamic forces are connected by linear dependence and have the same frequency [6].

The value of the variable aerodynamic force itself is not determining, it is much more important that its main frequencies (harmonic frequencies with maximum amplitude) do not coincide with the resonant frequencies of the elements of the flow path.

Conclusion

Thus, one of the goals obtained using the proposed technique is to find and determine possible dangerous frequencies of variable aerodynamic force acting on the rotor blades of the stage with a rotary diaphragm from the combination of the frequency spectrum of harmonics of the circumferential unevenness of the flow and the spectrum of natural frequencies of vibrations of the blades (a set of blades, the entire rim of the blades) in various modes of turbine operation.

A technique has been developed to determine the potentially dangerous frequencies of the variable aerodynamic force generated in front of the operating grid of the control stage with the rotary diaphragm in various modes of its operation.

The study, using the proposed method, of various operating modes of the rotary diaphragm, allows the obtained potentially dangerous frequencies for each operating mode, to be compared with the natural frequencies of the working rim of the control stage, and, in case of coincidence of these frequencies, either change the design and configuration of the windows of the rotary diaphragm, or structurally rebuild the blade apparatus from dangerous frequencies, or prevent such dangerous modes during turbine operation.

From all of the above, it can be concluded that the application of the procedure described in the article makes it possible to significantly improve the process of designing the turbine flow path.

Конфликт интересов

Не указан.

Рецензия

Сообщество рецензентов Международного научно-исследовательского журнала
DOI: <https://doi.org/10.23670/IRJ.2023.130.6.8>

Conflict of Interest

None declared.

Review

International Research Journal Reviewers Community
DOI: <https://doi.org/10.23670/IRJ.2023.130.6.8>

Список литературы / References

1. Левин А.В. Прочность и вибрация лопаток и дисков паровых турбин / А.В. Левин, К.Н. Боришанский, Е.Д. Консон. — Л.: Машиностроение, Ленингр. отд-ние, 1981. — 710 с.
2. Симою Л.Л. Расчет переменных режимов ЧНД теплофикационных паровых турбин / Л.Л. Симою, М.С. Индурский, Е.И. Эфрос // Теплоэнергетика. — 2000. — № 2. — С. 16-20.
3. Поздышев А.А. О повреждениях паровых турбин ТЭС / А.А. Поздышев, В.С. Рабенко // Вестник ИГЭУ. — 2004. — № 2.
4. Щегляев А.В. Паровые турбины. Учебник для вузов: в 2 кн. 6-е изд., переработанное, дополненное проф. Б. М. Трояновским / А.В. Щегляев. — М.: Энергоатомиздат, 1993. — 384 с.
5. Жинов А.А. Совершенствование регулирующих клапанов паровых турбин в трансзвуковой области течения: автореф. дис. ... канд. техн. наук / А.А. Жинов. — М., 1994.
6. Репецкий О.В. Факторы демпфирования вибрации лопаток турбомашин / О.В. Репецкий, В.М. Нгуен // Актуальные вопросы инженерно-технического и технологического обеспечения АПК: материалы IX Национальной научно-практической конференции с международным участием. — Молодёжный, 2021. — С. 134-141.
7. Ильичев В.Ю. Динамическое моделирование системы антипомпажного регулирования центробежного компрессора / В.Ю. Ильичев, В.Ю. Савин // Компрессорная техника и пневматика. — 2020. — № 2. — С. 34-38.
8. Ильичев В.Ю. Гармонический анализ сложного сигнала колебаний газотурбинного электроагрегата / В.Ю. Ильичев // Заметки ученого. — 2021. — № 12-2. — С. 82-86.
9. Галаев С.А. Численное моделирование нестационарного течения в последней ступени и выходном патрубке мощной паровой турбины / С.А. Галаев, А.И. Кириллов, В.В. Рис [и др.] // Научно-технические ведомости СПбПУ. Естественные и инженерные науки. — 2019. — Т. 25. — № 4. — С. 42-53.
10. Коркодинов Я.А. Обзор семейства $k-\epsilon$ моделей для моделирования турбулентности / Я.А. Коркодинов // Вестник пермского национального исследовательского политехнического университета. Машиностроение, материаловедение. — 2013. — Т. 15. — № 2. — С. 5-16.

11. Радин Ю.А. Определение допустимого регулировочного диапазона нагрузок энергоблока ПГУ-450Т при работе в конденсационном режиме / Ю.А. Радин, А.В. Давыдов, А.В. Чугин [и др.] // Теплоэнергетика. — 2004. — № 5. — С. 47-52.
12. Нгуен Нгок Т. Анализ резонанса и свободных колебаний лопатки газовой турбины / Т. Нгуен Нгок, В.М. Капралов // Научно-технические ведомости СПбПУ. Естественные и инженерные науки. — 2019. — Т. 25. — № 2. — С. 149-160.

Список литературы на английском языке / References in English

1. Levin A.V. Prochnost' i vibracija lopatok i diskov parovyh turbin [Strength and Vibration of Steam Turbine Blades and Discs] / A.V. Levin, K.N. Borishanskij, E.D. Konson. — L.: Mashinostroenie, Leningr. dep-ment, 1981. — 710 p. [in Russian]
2. Simoju L.L. Raschet peremennyh rezhimov ChND teplofikacionnyh parovyh turbin [A Calculation of the Variable Modes of the LDPEs of Heat and Power Steam Turbines] / L.L. Simoju, M.S. Indurskij, E.I. Jefros // Teplojenergetika [Thermal Energy]. — 2000. — № 2. — P. 16-20. [in Russian]
3. Pozdyshev A.A. O povrezhdenijah parovyh turbin TJeS [On Damage to Steam Turbines in Thermal Power Plants] / A.A. Pozdyshev, V.S. Rabenko // Vestnik IGJeU [Bulletin of ISEU]. — 2004. — № 2. [in Russian]
4. Shhegljaev A.V. Parovye turbiny. Uchebnik dlja vuzov: v 2 kn. 6-e izd., pererabotannoe, dopolnennoe prof. B. M. Trojanovskim [Steam Turbines. Textbook for Higher Education Institutions: in 2 vols. 6th edition, revised, supplemented by Prof. B.M. Troyanovsky] / A.V. Shhegljaev. — M.: Jenergoatomizdat, 1993. — 384 p. [in Russian]
5. Zhinov A.A. Sovershenstvovanie regulirujushhijh klapанov parovyh turbin v transzvukovoj oblasti techenija [Improving Steam Turbine Control Valves in the Transonic Flow Area]: abst. ... dis. PhD in Technical Sciences / A.A. Zhinov. — M., 1994. [in Russian]
6. Repeckij O.V. Faktory dempfirovaniya vibracii lopatok turbomashin [Vibration Dampening Factors for Turbomachinery Blades] / O.V. Repeckij, V.M. Nguen // Aktual'nye voprosy inzhenerno-tehnicheskogo i tehnologicheskogo obespechenija APK: materialy IX Nacional'noj nauchno-prakticheskoy konferencii s mezhdunarodnym uchastiem [Topical Issues of Engineering and Technological Support of Agro-industrial Complex: Proceedings of IX National Scientific-Practical Conference with International Participation]. — Molodjozhnyj, 2021. — P. 134-141. [in Russian]
7. Il'ichev V.Ju. Dinamicheskoe modelirovanie sistemy antipompazhnogo regulirovaniya centrobezhnogo kompressora [Dynamic Modelling of Centrifugal Compressor Anti-Pump Control System] / V.Ju. Il'ichev, V.Ju. Savin // Kompjutorsnaja tehnika i pnevmatika [Compressor Technique and Pneumatics]. — 2020. — № 2. — P. 34-38. [in Russian]
8. Il'ichev V.Ju. Garmonicheskij analiz slozhnogo signala kolebanij gazoturbinnogo jelektroagregata [A Harmonic Analysis of a Complex Oscillation Signal of a Gas Turbine Electric Unit] / V.Ju. Il'ichev // Zametki uchenogo [Notes of a Scientist]. — 2021. — № 12-2. — P. 82-86. [in Russian]
9. Galaev S.A. Chislennoe modelirovanie nestacionarnogo techenija v poslednej stupeni i vyhodnom patrubke moshhnoj parovoj turbiny [A Numerical Modelling of Unsteady Flow in the Last Stage and Outlet of a Power Steam Turbine] / S.A. Galaev, A.I. Kirillov, V.V. Ris [et al.] // Nauchno-tehnicheskie vedomosti SPbPU. Estestvennye i inzhenernye nauki [Scientific and Technical Bulletins of SPbPU. Natural and Engineering Sciences]. — 2019. — Vol. 25. — № 4. — P. 42-53. [in Russian]
10. Korkodinov Ja.A. Obzor semejstva $k-\epsilon$ modelej dlja modelirovaniya turbulentsnosti [Overview of the $k-\epsilon$ Family of Models for Turbulence Modelling] / Ja.A. Korkodinov // Vestnik permskogo nacional'nogo issledovatel'skogo politehnicheskogo universiteta. mashinostroenie, materialovedenie [Bulletin of Perm National Research Polytechnic University. Mechanical engineering, Materials Sciences]. — 2013. — Vol. 15. — № 2. — P. 5-16. [in Russian]
11. Radin Ju.A. Opredelenie dopustimogo regulirovochnogo diapazona nagruzok jenergobloka PGU-450T pri rabote v kondensacionnom rezhime [Determination of the Allowed Controlled Load Range of the CCGT-450T Power Unit when Operating in Condensing Mode] / Ju.A. Radin, A.V. Davydov, A.V. Chugin [et al.] // Teplojenergetika [Thermal Energy]. — 2004. — № 5. — P. 47-52. [in Russian]
12. Nguen Ngok T. Analiz rezonansa i svobodnyh kolebanij lopatki gazovoj turbiny [A Resonance and Free Vibration Analysis of a Gas Turbine Blade] / T. Nguen Ngok, V.M. Kapralov // Nauchno-tehnicheskie vedomosti SPbPU. Estestvennye i inzhenernye nauki [Scientific and Technical Bulletins of SPbPU. Natural and Engineering Sciences]. — 2019. — Vol. 25. — № 2. — P. 149-160. [in Russian]